

The simulation results are carried out using a commercially available software package HFSS, and the measured results are presented and discussed.

II. ANTENNA DESIGN

The geometry of the proposed printed slot antenna is shown in Fig. 1. The antenna is fabricated on FR4 substrate with a size of $35 \times 35 \times 1.6$ mm³, relative permittivity of 4.4, and loss tangent of 0.02. The radiating patch is in the shape of a fork and the slot, in the ground plane, has an elliptic shape. The printed slot antenna covers the UWB frequency range. By using elliptic-shaped quarter-wavelength stub in the ground plane, other practical frequency bands such as GSM band or Bluetooth band can be created.

The total length of the elliptic-shaped stub can be obtained approximately from the following formula:

$$L = \frac{c}{4f \sqrt{\frac{\epsilon_r + 1}{2}}} \quad (1)$$

where ϵ_r , c , and f are dielectric constant, the velocity of light in free space, and the center frequency of the added band, respectively.

By using two protrudent stubs in the ground plane, two additional tunable bands are created below the UWB band. Through optimization, the dimensions of the stubs can be obtained as follows:

$L_{S1} = 22$ mm (stub length related to GSM band), and $L_{S2} = 17$ mm (stub length related to Bluetooth band).

The final dimensions of the proposed triple-band slot antenna, as shown in Fig. 1 (a), are obtained as follows:

$R_1 = 3.5$ mm, $W_S = 35$ mm, $W_F = 2.5$ mm, $W_1 = 0.3$ mm, $W_2 = 2.5$ mm, $W_3 = 16.7$ mm, $L_F = 7$ mm, $L_S = 35$ mm, $L_1 = 3$ mm, $L_2 = 7$ mm, $L_3 = 10.6$ mm, $L_4 = 3.8$ mm, and $L_{S1} = 22$ mm, and $L_{S2} = 17$ mm.

III. RESULTS AND DISCUSSION

The simulated reflection coefficient of the proposed UWB printed slot antenna with and without the presence of elliptic-shaped stubs is shown in Fig. 2. As it can be seen the antenna without the elliptic-shaped stubs shows a good UWB response from 3.1 to 10.6 GHz. As shown in this figure, by creating an elliptic-shaped stub in the ground plane a new resonance is occurred below the UWB frequency range at 1.8 GHz (GSM band). Also by creating two elliptic shaped stubs two independent resonances can be created at frequencies of 1.8 GHz and 2.4 GHz (Bluetooth band) besides the UWB frequency band. The measured reflection coefficient of the proposed UWB printed slot antenna is shown in Fig. 3 as a comparison the simulated reflection coefficient is also shown in this figure. Good agreement between simulation and measurement results are observed.

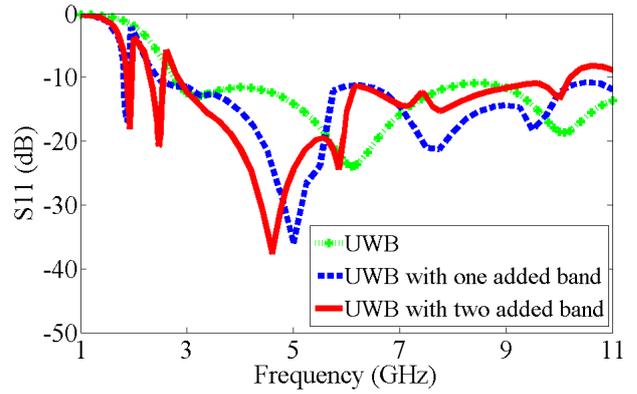


Fig. 2. Simulated S-parameters of the single band (UWB) antenna, dual band (UWB and one added band), and triple band proposed printed slot antenna.

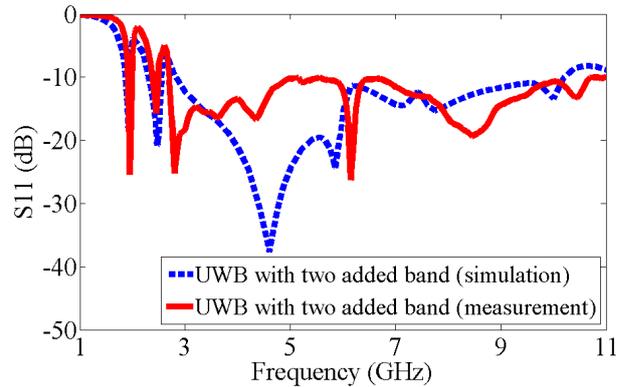
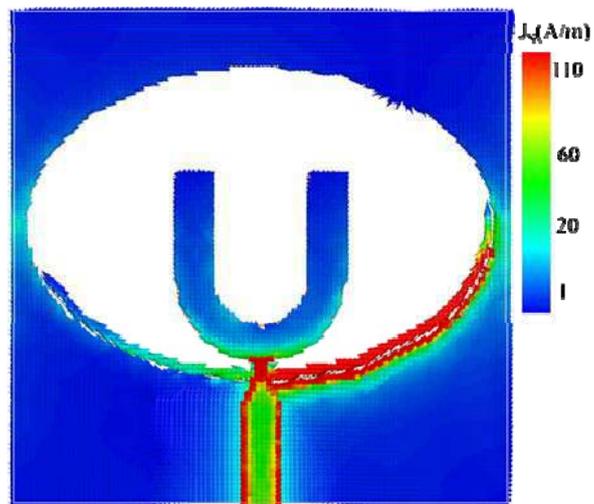


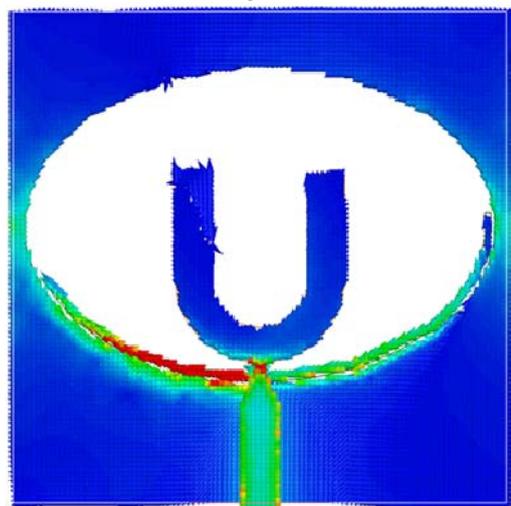
Fig. 3. Simulated and measured S-parameters of the proposed triple-band printed slot antenna.

For better understanding of the proposed antenna behavior, the current distribution on the antenna at frequencies of 1.8 GHz, 2.45 GHz, and 8 GHz is presented in Fig. 4. It is seen that at frequencies related to the added bands (e.g. 1.8 and 2.45 GHz) the current distribution is significantly high on the desired stubs. It is also seen from Fig. 4 (a), and (b) that the current distribution is maximum at one end and minimum at the other end of the stubs, proving the stubs are quarter-wavelength and confirms the validity of equation (1). On the other hand, one can see when one stub is activated the other stub is inactivated which shows the independency of added bands.

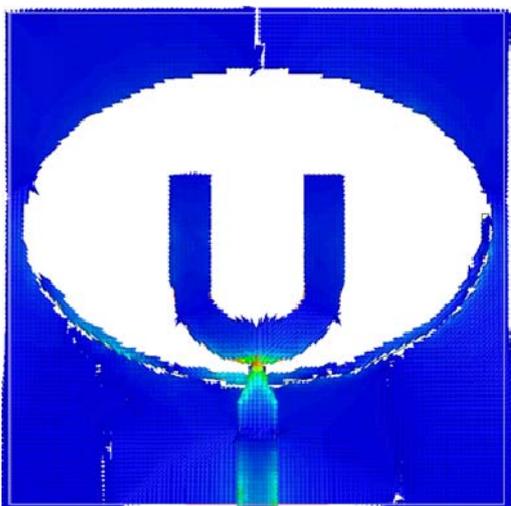
The measured radiation pattern of the proposed antenna in both E- and H-planes at three frequencies of 2.45, 4.5, and 6 GHz is shown in Fig. 5. As shown in Fig. 5, the antenna has almost stable omnidirectional radiation pattern in H-plane (x - z plane), and stable bidirectional radiation patterns in E-plane (y - z). The radiation patterns in both E- and H-planes are stable along the pass band frequencies. The simulated antenna radiation efficiency is shown in Fig. 6. It is seen that the antenna has good radiation efficiency in whole pass bands.



(a)

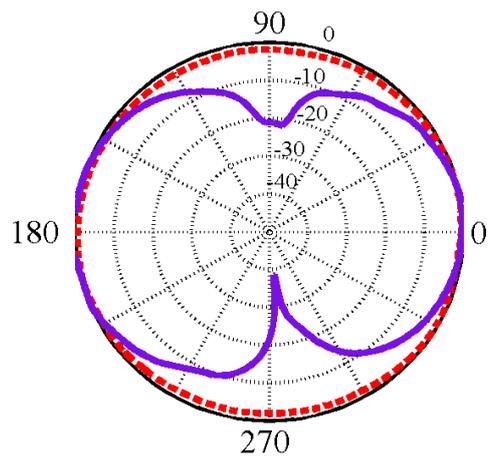


(b)

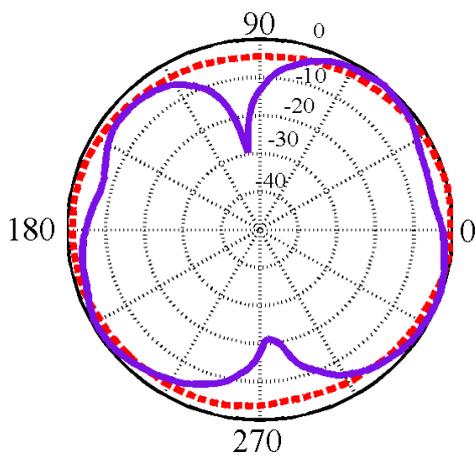


(c)

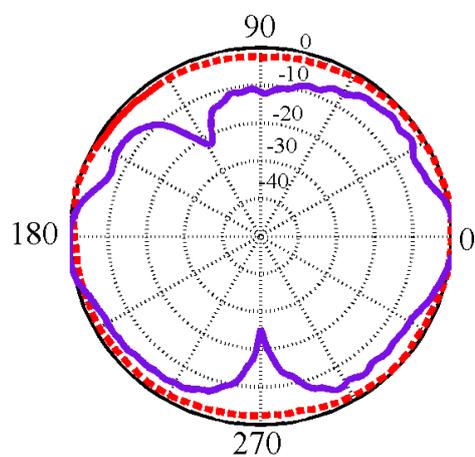
Fig. 4. Simulated current distribution proposed triple-band printed slot antenna at frequencies of (a) 1.8 GHz, (b) 2.45 GHz, and (c) 8 GHz.



(a)



(b)



(c)

Fig. 5. Measured radiation pattern (dB) of the proposed antenna at frequencies of (a) 2.45 GHz, (b) 4.5 GHz, and (c) 6 GHz. Dashed line represents H-plane ($x-z$ plane), and solid line represents E-plane ($y-z$ plane).

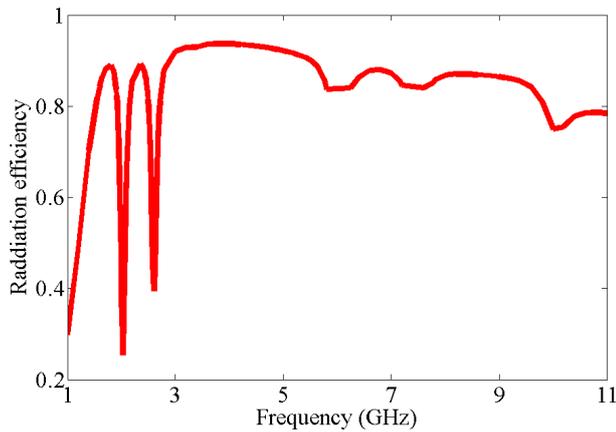


Fig. 6. The simulated antenna radiation efficiency

IV. CONCLUSION:

A Compact triple-band fork-shaped printed slot antenna for GSM, Bluetooth and UWB Applications is presented. The antenna has a compact size, stable radiation pattern and return loss of better than 10 dB over the whole of the triple bands.

References

- [1] R. Azim, M. Islam, N. Misran," Compact tapered shape slot antenna for UWB applications," *IEEE Antennas Wireless Propag. Lett.*, vol. 10, doi10.1109/LAWP.2011.2172181, 2011.
- [2] S. Cheng, P. Hallbjorner, and A. Rydberg, "Printed slot planar inverted cone antenna for ultrawideband applications," *IEEE Antennas Wireless Propag. Lett.*, vol. 7, pp. 18-21, 2008.
- [3] M.M. Samadi Taheri, H.R. Hassani, and S. Mohammad ali nezhad," UWB printed slot antenna with Bluetooth and dual notch bands," *IEEE Antennas Wireless Propag. Lett.*, vol. 10, pp. 255-258, 2011.
- [4] A. Foudazi, H. R. Hassani, S. Mohammad ali nezhad, " A dual-band WLAN/UWB printed wide slot antenna," *Antennas and Propagation Conference (LAPC)*, Loughborough, pp. 1-3, 2011.
- [5] B.S. Yildirim, B.A. Cetiner, G. Roqueta, and L. Jofre," Integrated Bluetooth and UWB antenna," *IEEE Antennas Wireless Propag. Lett.*, vol. 8, pp. 149-152, 2009.
- [6] S. Kumar Mishra, R. Kumar Gupta, A. Vaidya, and J. Mukherjee," a compact dual-band fork-shaped monopole antenna for Bluetooth and UWB applications," *IEEE Antennas Wireless Propag. Lett.*, vol. 10, pp. 627-630, 2011.